



Performance of an innovative gravity-driven micro-filtration technology for roof rainwater treatment

Chen Shiguang[†], Sun Hongwei, Chen Qiuli

College of Urban and Rural Construction, Zhongkai University of Agriculture and Engineering, Guangzhou 510225, China

Abstract

Rainwater harvesting has become an important strategy to achieve the goal of sustainable development in urban areas. The latest emerged gravity driven micro-filtration technology can effectively reduce turbidity and bacteria to a very low level but still have disadvantages of low removal of dissolved organic substances and low permeate flux. An innovative gravity driven micro-filtration technique using ceramic flat sheet membrane as filter module was established and introduced to the treatment of rainwater that was harvested from a typical official building in GuangZhou, South China. The performance of this process has been evaluated in terms of pollutants (e.g. pH, turbidity, total dissolved solids (TDS), COD_{Cr}, NH₃-N, DOC, UV₂₅₄, total *Coliforms* and *E.coli*) removal efficiency, and the permeate flux profiles. Results shows that the removal rates of turbidity, TDS, COD_{Cr}, NH₃-N, DOC, UV₂₅₄, *Coliforms* and *E.coli* were 92.2%, 91.9%, 65.5%, 42.6%, 76.9%, 61%, 96.9% and 95.5%, respectively. The GDM system can run continuously for 60 days without back washing, and the permeate flux stabilized at 22~45 L/(m²·h) under a constant water head of 20 kPa. Experimental results demonstrated that the GDM system employing a ceramic flat membrane can significantly improve the organics removal in rainwater.

Keywords: Ceramic membrane, Harvesting, Micro-filtration, Rainwater



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[†] Corresponding Author

E-mail: luyi813929@163.com

Tel: +86-20-89002673 Fax: +86-20-89002673

ORCID: 0000-0002-4102-6886

1 **1. Introduction**

2 Most urban areas around the world have witnessed rapid population growth and are confronted
3 with the issue of supplying adequate water to satisfy the demand of social consumption and
4 economic activities [1]. Rainwater and stormwater recycling offer promising alternatives to
5 address water supply pressures in areas where water sources are scarce or polluted [2]. The reuse
6 of rainwater enables a reduction in the consumption of potable water, thus saving fresh water
7 resources, reduce energy intensity, diminishing stormwater runoff and combined sewer overflows
8 [3-6].

9 Nevertheless, until recently, widespread implementation of rainwater harvesting systems
10 in urban areas have not yet emerged [7]. Public health concern is considered to be one of the
11 main obstacles for rainwater and stormwater reuse [8]. Although rainwater is generally of a high
12 quality (COD < 200 mg/L), rainwater in the urban area still contains a certain amount of
13 contaminants including particles, microorganisms and organics [9]. Therefore, further treatment
14 of the collected rainwater is necessary for the supply of safe and sanitary water for potable or
15 non-potable use. Various methods of treating rainwater for the non-potable use have been
16 widely adopted, such as chlorination, pasteurization by solar technology, biofiltration, membrane
17 separation, etc [10, 11].

18 Emerged as a low energy consumption and chemical free technology, the gravity driven
19 membrane (GDM) filtration process is receiving more attentions and has been introduced to treat
20 rainwater prior to use [12-14]. Although the GDM process has demonstrated an excellent
21 performance in removing the bacteria and suspended particles in surface water and wastewater
22 treatment, however, this energy-saving technology still has some disadvantages, such as, the

1 removal of low molecular-weight substances is not ideal [15]. Thus, new technologies targeting
2 to improve the dissolved organic matter removal in GDM systems need to be explored.

3 In the design of GDM filtration process, the selection of filter media is of critical
4 importance, as is related to the removal efficiency of pollutants, initial costs and permeate fluxes
5 [16]. As a new filter material, micro-porous ceramic has lower density and higher specific
6 surface area as compared to conventional micro-filtration membrane media such as cellulose
7 acetate, polyvinylidene fluoride (PVDF), and polyethersulfone (PES) [17]. The ceramic filter has
8 been reported to satisfactorily remove different pollutants in drinking water treatment, i.e., 40-58%
9 for TOC and more than 70% for nitrogen [18, 19]. These signify that employing ceramic
10 membrane is very likely to achieve the desired results in rainwater treatment which has not been
11 reported to date.

12 Most previous studies on GDM technologies have focused on the organic hollow fibre
13 membranes probably linked to the hypothesis that a higher packing density of the membrane
14 module is assumed to achieve more productivity per unit of footprint [20]. However, it is noted
15 that, compared to the hollow fibre membrane modules, the flat sheet membrane modules, can
16 offer superior environment for the growth, movement and predation behaviour of eukaryotic in
17 the bio-fouling layer, which is responsible for the reduction of bio-fouling layers on the
18 membrane, (i.e., form an open, heterogeneous, and porous fouling layer), and consequently
19 contribute to a relatively higher level of permeate flux. Moreover, since previous studies have
20 stated that membrane fouling was primarily due to the deposition of soluble microbial products
21 such as polysaccharides, proteins, and fulvic substances onto the membrane surface [21, 22], the
22 ceramic membrane, which possesses properties of higher hydrophilic, thus has the potential to

1 prevent the formation of cake layer (because hydrophilic membrane can effectively prevent those
2 substances from migrating to the membrane surface). Such characteristic offers a possibility to
3 improve the overall permeate flux of GDM system.

4 Nevertheless, whether a flat sheet ceramic membrane can benefit to improve the removal
5 efficiency of DOC or to enhance the productivity of the GDM systems for rainwater treatment is
6 to date not been reported. Therefore, the objective of this study is to assess the performance of
7 ceramic flat membrane in rainwater filtration. An innovative GDM filtration system using
8 ceramic flat membrane as filter module was designed and used for the rainwater treatment in an
9 official building located in Guangzhou, South China. The pollutants removal efficiency was
10 investigated in terms of pH, turbidity, total dissolved solids (TDS), COD_{Cr}, NH₃-N,
11 DOC, UV₂₅₄, total *Coliforms* and *E.coli*, and the impacts of flat sheet membrane on GDM
12 permeate flux development were also evaluated. It should be point out that, the current work is
13 specific to study site, the results obtained may vary from one location to another due to the the
14 quality of rainwater depends on rainfall amount, the type of roof and storage material adopted etc.

16 **2. Material and Methods**

17 This section presents the study site, the materials used, the description of the RWH system, the
18 GDM process, and the analytical methods employed in this study.

20 **2.1. Study site**

21 The study site (with latitude 23°37' north and longitude 113°44' east), locates on the North edge
22 of the Pearl River Delta (PRD) Plain in the province of Guangdong in southern China, which,

1 according to the classification, has a typical subtropical monsoon climate, and the average annual
2 precipitation is around 1,790 mm (statistical average from 1980s~2010s).The average annual
3 temperature is 22.5°C with no frost or snowfall. The location map of study site is presented in the
4 supplementary materials (named Fig. S1).

5

6 **2.2. Materials**

7 The raw-rainwater used in this study was harvested from a planted roof of an eight-story multi-
8 functional building (with catchment area of 1,122 m²). The GDM device was designed and
9 manufactured by Shen Zhen Jingrui 3D Printing Co.,Ltd (Shenzhen, China). Flat-sheet ceramic
10 membranes with multi-channels (ZhongQing Environmental Technology Co.,Ltd, Shenzhen,
11 China) were used in this study. They are made from alpha-alumina with a nominal pore size of
12 0.1 μm. Each membrane has a dimension of 520 × 200 × 4 mm (L × W × H) corresponding to a
13 filtration area of 0.21 m² (double side inlet). The flat sheet ceramic membrane
14 has the characteristics of high structural strength, excellent durableness (it can operate under
15 extremely harsh conditions such as strong acid, strong alkali and high temperature), and low
16 maintenance costs due to no backwashing and chemical cleaning.

17

18 **2.3. RWH Systems**

19 The RWH system consists of four main elements: (1) Catchment surface: Rooftop (1,122 m²). (2)
20 Storage facilities: A raw-rainwater tank installed below roof, and an effluent tank (Fig. 2) to
21 temporary store water before use. (3) The gravity driven micro-filtration treatment unit. (4)
22 Delivery system: Set of pipes that transport rainwater from the catchment area to the storage tank

1 and then from the storage tank to effluent tank and ultimately sent to the end users of the
2 building. The treated rainwater was mainly used for toilet flushing, hand washing and laundry.
3 The schematic diagram of RWH system can be found in supplementary materials (named Fig.
4 S2).

6 **2.4. Process Operation**

7 The schematic view of the GDM reactor is shown in Fig. 1. Before filtration, harvested rainwater
8 was temporary stored in a raw rainwater tank. Excesses of rainwater were discharged by gravity
9 drainage through overflow pipe when the collected rainwater exceeded the capacity of the
10 storage tank, while a float valve was used to ensure that the level of rainwater inside the tank
11 does not go below a certain threshold level during periods without rainfall (Fig. 1).

12 The rainwater was first screened with a 0.55 mm sieve to remove large suspended
13 particles, then fed into the membrane tank at a controlled rate that synchronised with the filtrates
14 withdrawal. A 20 kPa (2 m) gravitational head generated from the height between the raw-
15 rainwater tank and the effluent tank was utilized to drive the rainwater flow through the
16 membrane filter (Fig. 1). After filtration, the treated rainwater was temporary stored in the
17 effluent tank for distribution. The GDM system operated in a dead-end filtration mode, and the
18 running duration of the system was 60 days (from June 12 to August 14, 2019) with a primarily
19 flux of 168 L/m²·h. The average hydraulic retention time (HRT, which is calculated by dividing
20 reactor volume by permeate flow rate) in the membrane tank was 7.63 h.

22 **2.5. Analytical Methods**

1 During the experiments, samples obtained from the feed tank, and effluent tank were analyzed
2 regularly for pH, total dissolved solids (TDS), turbidity, ammonia nitrogen (NH₃-N), chemical
3 oxygen demand (COD_{Cr}), dissolved organic carbon (DOC), UV254. For microbiological
4 parameter all samples were examined for the two widely used bacterial indicators, total
5 *Coliforms*, and *Escherichia coli*. The pH was determined by a Phs-3c precision pH meter
6 (Rex Electric Chemical, China), and the turbidity was measured using a 2100P Portable
7 Turbidity meter (HACH, USA). TDS was determined by gravimetric method according to the
8 Standard Methods for Examination of Water and Wastewater [23]. DOC was measured by using
9 the Multi N/C 2000 analyzer (Analytik Jena AG). COD_{Cr} was determined by a DR-1010 COD
10 rapid Monitor (HACH, USA) and NH₃-N was measured using a 722 spectrophotometer
11 (Shimadzu, Japan), while UV254 was monitored by an uv-2450 ultraviolet spectrophotometer
12 (Shimadzu, Japan) in terms of UV absorbance at the wavelength of 254 nm. For *Total Coliforms*
13 and *E. coli* analyses the methods outlined in APHA (2005) were adopted. Acetate cellulose
14 filters (0.45 μm poresize, Biocomma, China) were used for sample filtration while m-Endo Broth
15 medium (Shanghai binsui Biotechnology Co., Ltd, China) and Tryptone Bile X-Glucuronide
16 (TBX) medium (Shanghai Zeye Biotechnology Co., Ltd, China) were employed respectively for
17 *Coliform* and *E.coli* retention. The results were expressed in terms of colony forming units per
18 100 mL (CFU/100 mL). The measurement frequencies for pH, turbidity, TDS, COD_{Cr}, NH₃-N,
19 UV254, dissolved organic carbon (DOC) were once a day, while for *Coliform* and *E.coli* were
20 once every three days. The measurements were made thrice each time.

21 A PZ-M digital camera of biological microscope (Shanghai Optical Instrument
22 Factory, China) was used as an in situ method to capture the morphologies of microorganisms on

1 the membrane surface of the GDM reactor. These measurements were conducted on the first day,
2 the 20th day, the 40th day and the 60th day of the experiment.

3

4 **3. Results**

5 Laboratory experiments monitored the daily water quality and flux decline from the GDM filter
6 system. The following sections report representative results obtained during 60 days experiment.

7

8 **3.1. Analysis of Effluents Quality**

9 Table 1 compares the quality of influent rainwater and effluent from GDM system. All
10 parameters monitored in this experiment are compared against the limits of Chinese Recycling
11 Water Guidelines (CRWG,2014) [24] and Chinese Drinking Water Guidelines (CDWG,2006)
12 [25], respectively.

13 The results showed that the rainwater collected in study site generally complied with the
14 limits of CRWG (2014) except for parameters such as the turbidity, COD_{Cr}, and bacteria (Table
15 1). This may due to the fact that the sampling site is far away from the urban area and less
16 polluted by automobile exhaust or industrial emissions.

17 As shown in Table 1, the pH value of feed rainwater ranged from 6.4 to 8.1, with an
18 average value of 7.4, and the pH range of effluent from GDM reactor was 6.7-8.3 over the entire
19 experimental period. The effluent pH value were in compliance with the CRWG (2014) and
20 CDWG (2006), in which the permissible limit for pH should be in the range of 6.5-9.0 and 6.5-
21 8.5, respectively.

1 During the experiments, the turbidity in the raw rainwater ranged from 4.22 to 7.50 NTU (or
2 5.86 ± 1.64 NTU on average, as shown in Tab.1). The CRWG (2014) has a recommended limit
3 for turbidity of 5 NTU, therefore the raw rainwater concentration of turbidity was in most cases
4 beyond the CRWG limit. The gravity driven micro-filtration (GDM) system, reduced the
5 turbidity by an average of 92.2%, to a levels of 0.46 ± 0.33 NTU, with the effluent turbidity well
6 complied with the Chinese Drinking Water Guidelines (2006), which prescribed the turbidity <
7 1.0 mg/L. The low effluent turbidity from GDM reactor was expected due to the filtration
8 function of ceramic membrane that with pore size of 0.1 μm . Since most of the suspended
9 particles in rainwater were more than 0.1 μm in diameter, therefore, negligible amount of
10 turbidity related pollutants can penetrate ceramic membrane of the GDM reactor.

11 Table 1 also compares the TDS concentration of feed rainwater and effluent from GDM
12 unit. The TDS in the stored rainwater fluctuated between 33.6 and 384.4 mg/L, while the effluent
13 TDS ranged from 6.7 to 27.3 mg/L, much lower than the limit of the Chinese Drinking Water
14 Guidelines (< 1,000 mg/L). The TDS removal was mostly above 90% with an average removal
15 rate of 91.9% over the experiment period.

16 Two bacterial indicators, total *Coliform* and *E. coli* were detected to reflect the
17 microbiological variables of rainwater. The feed rainwater contains total *Coliforms* an average
18 value of 128 CFU/100mL within a range of 91 to 165 CFU/100 mL, and contains *E.coli* an
19 average value of 330 CFU/100 mL within a range of 188 to 472 CFU/100 mL (Tab.1). In current
20 study, the influent *Coliforms* and *E.coli* concentrations in rainwater were somewhat lower than
21 the reported range of previously literatures (i.e. typically 10-12,000 CFU/100 mL for coliforms
22 and 0-3,200 CFU/100 mL for *E.coli*, respectively [26]. This probably linked to the seasonal

1 fluctuations of microbiological parameters which were affected mainly by the cleanness level of
2 catchment areas. In GDM effluent, the *Coliform* concentrations were ranged from 0 to 9
3 CFU/100 mL, and the *E.coli* were ranged from 0~30 CFU/100 mL (seen Tab.1), approximately
4 95% of *bacteria* in the rainwater were removed. Whereas the CDWG (2006) suggests non-
5 detectable *Coliform* and *E.coli* per 100 mL, while CRWG (2014) suggests no more than 100
6 *Coliform* and *E.coli* per 100 mL, therefore the bacteria concentration in the treated water well
7 satisfy the non-potable water standard and in most cases meets the drinking water standard.

8 According to the results, in GDM reactor, the effluent concentrations of $\text{NH}_3\text{-N}$ were 3.21
9 ± 1.56 mg/L, the effluent COD_{Cr} were ranged from 8.0 to 16.8 mg/L, whereas the effluent DOC
10 were between 1.66 and 2.68 mg/L, the effluent UV₂₅₄ of rainwater were 0.034 ± 0.018 cm⁻¹.
11 The rejection of $\text{NH}_3\text{-N}$, and UV₂₅₄ by the 0.1 μm ceramic membrane was 42.6% and 61%, and
12 the removal of COD_{Cr} and DOC were 65.5% and 76.95, respectively, which were far less than
13 those of turbidity, TDS, and bacteria, the latter have demonstrated a rejection of 92.2%, 91.9%
14 and 95%, respectively. The diversity of particle size could be responsible for the difference in
15 removal efficiencies among various physicochemical parameters.

16 As known to remove contaminants mainly through filtration, the GDM system has its
17 removal efficiency generally increases with decreasing nominal pore size of membranes.
18 Theoretically, the pollutants with diameter less than 0.1 μm cannot be rejected through micro-
19 filtration process. Since the sizes of dissolved organic matters are generally less than 100nm in
20 diameter [27], therefore, majority percentage of these small molecule contaminants would not be
21 rejected by GDM system. However, it was observed that there were still more than half of $\text{NH}_3\text{-}$

1 N, COD_{Cr} and DOC in rainwater were removed by ceramic membrane in current GDM filtration
2 system, this hinted that some supplementary mechanisms occurred during the filtration process.

3

4 **3.2. NH₃-N and Organics Removal**

5 Fig. 2 illustrated detailed NH₃-N concentrations of the feed rainwater and effluent from GDM
6 system during the experimental period. The average NH₃-N concentration of the effluent
7 throughout the experimental period was 3.21 mg/L, corresponded an average removal rate of
8 42.6%, with the effluent quality well below the Chinese Recycling Water Guidelines limit of 10
9 mg/L, but beyond the Chinese Drinking Water Guidelines limit of 0.5 mg/L. As can be seen
10 from Fig. 2, it was obviously that the removal efficiency of ammonia nitrogen by GDM system
11 seem to be slightly higher in the later period of operation, e.g., the effluent concentrations of
12 NH₃-N were fluctuated between 2.53~4.77 mg/L in the first 30 days, corresponding to average
13 removal rate of 33.6%, and ranged of 3.32 to 4.63 mg/L from day 31 to day 46, corresponding to
14 average removal rate of 44.3%, while over the final 14 days of the experiment, the effluent NH₃-
15 N concentrations were in the range of 1.65~3.22 mg/L, corresponded an average removal rate of
16 57%.

17 Fig. 3 compares the COD_{Cr} concentrations in feed rainwater and filtrates from GDM
18 reactor. It can be seen from Tab.1 that chemical oxygen demand (COD_{Cr}) in raw rainwater were
19 35.9±15.6 mg/L, with maximum value exceeded the recommended limit (< 50 mg/L) of Chinese
20 Recycling Water Guidelines. As shown in Fig. 3, a great part of COD_{Cr} in the raw rainwater was
21 removed after GDM treatment that achieved an effluent COD_{Cr} between 8~16.8 mg/L, well
22 below the Recycling Water limits but slightly exceeded the standards for drinking water quality,

1 contributed an average reduction of 65.5%. Nevertheless, previous studies have reported that the
2 organic matters cannot be effectively removed by micro-filtration process, as stated by Ding et al.
3 [15], the removal rate of organic matter by micro-filtration process was lower than 20%, this
4 discrepancy with current study may be attributable to the differences in properties of membrane
5 adopted. Our observations demonstrated that in case of rainwater treatment, the GDM process
6 using ceramic membranes enables a considerable reduction in these pollutants that cause COD_{Cr}.
7 Presumably this may linked to the biological process that occurred on the ceramic membrane
8 surface due to the formation of a bio-film as the experiment were prolonged.

9 Fig. 4 and Fig. 5 illustrate the comparison of influent and effluent rainwater from GDM
10 system in term of water quality parameters of DOC and UV254, respectively. As listed in Table
11 1, the influent rainwater samples contained an average dissolved organic carbon (DOC) of $9.4 \pm$
12 3.86 mg/L. According to Fig. 4, the GDM system removed majority of the dissolved organics
13 matters that gave a final effluent DOC concentrations of 2.17 ± 0.51 mg/L or 76.9% removal
14 efficiency. The influent rainwater samples contained UV254 a range of 0.087 ± 0.024 cm⁻¹, and
15 the GDM treatment reduced the UV254 to a level of 0.034 ± 0.018 cm⁻¹, which resulted in a
16 greater than 61% reduction. Therefore, it can be concluded that great parts of DOC and UV254
17 were removed from feed rainwater through this GDM system. As for the micro-filtration
18 processes, the effects are usually associated with the pore size of the membrane, whereas the
19 nominal pore size of the micro-filtration membrane (0.1 μm) is far greater than those of
20 dissolved organic matters, therefore most of the dissolved organic matters that cause DOC and
21 UV254 in the rainwater cannot be rejected by alone micro-membrane. It is assumed that the
22 removal of dissolved organic matters may be on one side imputable to the adsorption by porous

1 ceramic membrane, and on the other hand linked to the flat sheet membrane that can offers a
2 desirable surface for the attachment of microbial communities, which can also help to reduce the
3 DOC contents through bio-degradation.

4 As can be seen from Fig. 4, the effluent concentrations of DOC were found lower in later
5 stage of experimental operation. These observations were well in agreement with the
6 aforementioned hypothesis that the removal of dissolved organic matters was resulted from the
7 conjoint effects of adsorption by ceramic membrane and degradation by the bio-film on the
8 membrane surface (detailed reasons will be presented in the section of discussion).

9

10 **3.3. Membrane Morphology**

11 The micrograph of microbial communities derived from the settlements of membrane surface
12 were captured through a light microscope (Fig. 6(a)-(d)). As obvious, substantially eukaryotic
13 microorganisms were observed on membrane surface. Under the microscope, these eukaryotic
14 microorganisms are rod, or filamentous shapes, their sizes range from nearly one hundred
15 micrometers to a few millimetres in length. This phenomenon may be attributed to the fact that
16 in the GDM filtration reactor, a large number of microorganisms (consist of bacteria and
17 eukaryotes) from the feed rainwater were retained due to membrane rejection, and the bacteria
18 utilize the organic substances in the feed water for their growth and then form bio-film layers on
19 the membrane surface. These bio-films may play important role in removing of pollutants
20 especially degradable organic matter from rainwater. During current experiment, it is evident that
21 there were abundant microorganisms gathered on the membrane surface and were growing

1 during the long term filtration, making this GDM process evolved into a membrane bio-reactor
2 (MBR), thus contributed to the degradation of organic substances.

3 As can be seen from Fig. 6, the biomass in the later stages (i.e., by the end of 40th and
4 60th day, respectively, seen Fig. 6(c), (d)) were much higher than the early stages (Fig. 6(a), (b)).
5 These observations were also consistent with the the aforementioned results (section 3.2) that the
6 removal efficiency of ammonia nitrogen were improved in the later stage of the experiment.

8 **3.4. Flux Development Profiles**

9 The recorded flux development profiles of GDM reactors over a duration of 60 days are
10 illustrated in Figure 7. For the planted roof rainwater filtration, the initial permeate fluxes of
11 GDM reactor were desirable but it dropped rapidly with increasing running duration. After 10
12 days, the permeate flux of ceramic membrane declined to $60 \text{ L/m}^2 \cdot \text{h}$, approximately 36% of its
13 initial level. It can be inferred that pore blocking may have occurred at the very beginning of
14 operation, which caused permeate flux decline in the ceramic membrane GDM system.

15 Previous studies have documented that membrane fouling was primarily due to the
16 deposition of soluble microbial products such as polysaccharides, proteins, and humic and fulvic
17 substances onto the membrane surface or into membrane pores [28-30]. Therefore, it was
18 expected that the permeate flux would further decline with the experiment prolonged since the
19 cake layer has developed in the membrane surface without any backwashing and chemical
20 cleaning. However, it was observed that the flux downward trend appeared to be moderate after
21 14 days, which was approximately equivalent to 45 h (it is noteworthy that the GDM reactor was
22 operated at an intermittent mode of 2-4 h a day). The permeate flux of the GDM unit declined to

1 a relative stable level that ranged between 22 and 47 L/m²·h. Apparently, as shown in Fig. 7, the
2 permeate flux profile of the current GDM reactor can be roughly categorized into two stages, the
3 first stage was from the first day to 14th day, while the later stage spanned from the 14th day
4 until to the end of the experiment.

5 Similar decline patterns have also been documented in some previous studies that
6 employed seawater [31, 32], surface water [33], grey water [34], and waste water as feed waters
7 in micro-filtration systems. However, flat ceramic membrane with 0.1 μm pore size shows much
8 slower permeability decline, and the stabilized permeate fluxes were significant higher than
9 those of previous studies documented, e.g, several studies have reported that the permeate fluxes
10 of GDM filtration process were typically lower than 10 L/m²·h, with most ranged from 3.6 to
11 14.9 L/m²·h [31-33, 35]. It is noted that the GDM system was not backwashed over an
12 experimental duration of 60 days, although the flux can be recovered easily by hydraulic
13 cleaning since Tang et al. have reported that more than 75% of membrane resistance comes from
14 reversible fouling [29].

15 According to the findings by Peter et al. [33], the stabilization of flux was related to the
16 development of heterogeneous structures in the bio-fouling layer on the membrane surface, and
17 the level of stable permeate flux depended on the ATP and EPS contents of bio-fouling layer
18 rather than the DOC concentration in the feed water. Therefore the high stabilized permeate
19 fluxes in our experiment can only be partially attributed to the feed rainwater that contain fewer
20 amounts of dissolved organic pollutants, even more importantly, the high fluxes may have
21 mainly resulted from the hydrophilicity of the ceramic membrane, which lead to less
22 accumulation of polysaccharides and proteins on the membrane surface, thus to lighten

1 membrane fouling and clogging, then resulting in a higher permeate flux. In addition, the flat
2 sheet membrane (compares with the hollow fiber membrane) provides a superior environment
3 for the growth, predation, and movement of the eukaryotes or predators, which also contribute
4 to resist the development of cake layer on membrane surface.

5

6 **4. Discussion**

7 In this study, a 60 days experiment was conducted to evaluate the performance of an innovative
8 gravity driven ceramic membrane micro-filtration process for harvested rainwater treatment.
9 Results shows that the treatment system reduced all the tested pollutants to below the limits of
10 the Chinese Recycling Water Guideline (2014). Several parameters such as turbidity, TDS and
11 bacteria even met the Chinese drinking water standard (2006), more importantly, without any
12 backwashing throughout the entire experiment.

13 The performance of the GDM system in terms of the removal of several pollutants has
14 been discussed in the previous sections. As pointed out elsewhere, the GDM process may exhibit
15 excellent performance for bacteria and turbidity removals, but the removal efficiencies of
16 organic matter and ammonia nitrogen were undesirable [36-39]. For example, Peng and
17 Diamantis have reported that the micro-filtration were capable to remove majority of the
18 suspended solids, colloidal particles and pathogens, but the removal rate of dissolved organic
19 matters by alone micro-filtration process was generally lower than 20% [40, 41]. While Kus et al
20 observed that a GDM process only contribute to 7% removal efficiency of DOC [42]. Similarly,
21 Wu et al have recorded that a pilot GDM systems were able to remove almost all of the particles
22 (i.e., turbidity), 94% of viable cells, and most of TEP (41-85%) [43]. However, Ding et al reveal

1 that DOC (especially the organics containing unsaturated bonds or aromatic chromophores) of
2 rainwater were not removed well (lower than 30%) in GDM process [15]. Whereas in another
3 study, Wu et al also found that GDM did not retain humics and low molecular weight neutrals
4 during sea water treatment [32].

5 However, in current study, the average removal rate of DOC in GDM system was 76.9%,
6 which was significant higher than those of most previous researches documented. In addition, the
7 removal of GDM system for other organic pollutants as well as ammonia nitrogen were also
8 satisfying, through GDM filter, averagely 65.5% removal of COD_{Cr}, 42.6% removal of NH₃-N,
9 and 61% removal of UV₂₅₄ were achieved, respectively.

10 The relatively high efficiencies of the current GDM system in reducing dissolved organic
11 matter and NH₃-N could be attributed to two reasons. First, the ceramic membrane is a filter
12 media with superior hydrophilicity. This characteristic allow the GDM system to run for a
13 relative longer period without cleaning, and thereby it would favor various of microorganisms to
14 accumulate and form a bio-film over the membrane surface, which consequently favours
15 biodegradation in the GDM reactor, as a consequence, leading to a reduced concentration of
16 dissolved organic matters retained in the treated rainwater. As found in our previous study, the
17 ceramic membrane can integrates the coagulation, precipitation, adsorption, advanced oxidation,
18 biological treatment and other processes, which can effectively remove organic matters [44]. It
19 was noted that the membrane adopted in current experiment has a nominal pore size of 0.1 μm,
20 therefore, theoretically the substances < 0.1 μm cannot be rejected by the membrane. However,
21 when the rainwater filtered through the membrane, these soluble substances could be adsorbed to
22 or captured by the bio-film layer on the membrane, parts of organic fractions were assimilated

1 and utilized as carbon source for microorganisms proliferation [11], thus enables a reduced DOM
2 contents in effluent from GDM reactor. As can be seen from Fig. 2, Fig. 3, Fig. 4 and Fig. 5, the
3 removal efficiency of GDM system for $\text{NH}_3\text{-N}$, COD_{Cr} , DOC and UV254 appeared to be slightly
4 higher after 40 days operation, e.g. the effluent $\text{NH}_3\text{-N}$ concentrations were ranged from
5 2.53~4.77 mg/L in the first 30 days, then down to 1.65~3.22 mg/L from day 47 to the end (Fig.
6 4). This phenomenon may be as a result of the continuous operation of the GDM reactor, which
7 could favor the attachment of nitrobacteria that possess longer growth period on the ceramic
8 membrane surface, and consequently lead to nitrification taken place in the GDM reactor, thus
9 benefit to the removal of ammonia nitrogen. Second, a proper water temperature (between 23.3°C
10 and 28.2°C) also promoted the degradation of organic compounds. Previous study shows that the
11 activity of microorganism reached maximum at a temperature range of 25 to 35°C, while the
12 activities of microorganism and the hydrolysis rate may decline when the temperature drops [45].

13 The observation that the increase in organic removal was related to the microbial
14 biodegradation is also agreed with the findings in previous studies [30, 46]. The cake layer
15 formed on the surface of membrane has been reported to lead to a quality improvement of
16 drinking water filtration system [47, 48]. As pointed out by Vincenzo et al. [46] (2013), in the
17 filtration system of surface water, due to long-term operation of the filter, microorganism such as
18 bacteria, protozoa and metazoa have opportunities to accumulate on the membrane surface, thus
19 to form a biofilm with bioactivity, resulting in the biodegradation of soluble organic constituents.

20 In addition to the aforementioned aspects, the higher organic matter removal rate may be
21 linked to the longer hydraulic retention time of the GDM reactor, since the HRT in the later stage
22 was increased due to the decline of permeate flux. Prior studies have noted that longer hydraulic

1 retention time would favour the growth and proliferation of microorganisms on membrane
2 surface, especially eukaryotes, which could result in a bio-film with higher biomass and
3 greater diversity [43], whereas the HRT of the GDM reactor is mainly determined by the size of
4 GDM reactor (HRT, is calculated through dividing reactor volume by flux rate). These findings
5 hinting that the reactor dimension is an important factor determining both organic degradation
6 and development of the bio-film on the membrane surface of the GDM filter tank. Therefore,
7 Follow-up investigations are planned to optimize this parameter in order to achieve higher
8 removal efficiency with lower maintenance.

9 In terms of permeate flux, the stabilized flux was at 22~45 L/m²·h over 60 days
10 experiment, which was significantly higher than that of previous study documented, e.g., Bing
11 Wu (2017) have reported that stabilized permeate flux of 16.3 to 18.6 L/m²·h were achieved at a
12 hydrostatic pressure of 200 mbar by hollow fibre membrane reactor after two months operation
13 [43]. This is possibly attributed to the fact that, compared to the hollow fiber membrane, the flat
14 sheet membrane module provides more space for the predation and movement of some
15 eukaryotes that were growing and propagating in the GDM reactor, since the movement and
16 predation behaviour of eukaryotic organisms have been reported to produce the porous, sponge-
17 like structures of biofilm, which benefits to the improvement of permeate flux [43].

18 Although the current study is specific to study site, however, this paper presents an
19 insight on potential advantages of GDM system using flat ceramic membrane for rainwater
20 treatment and such study will motivate others to conduct similar investigations in elsewhere.

21

22 **5. Conclusions**

1 The ceramic membrane was employed in a GDM system to treat harvested rainwater at Lab-
2 scale. Results showed that this process presented excellent performance in term of pollutants
3 removing and permeate flux. The average removal rate of turbidity, TDS, COD_{Cr}, NH₃-N, DOC,
4 UV254, *Coliforms* and *E.coli* by the GDM system was 92.2%, 91.9%, 65.5%, 42.6%, 76.9%,
5 61%, 96.9% and 95.5%, respectively, with all surveyed parameters meeting the standards for
6 non-potable purpose. The permeate flux of the GDM system dropped rapidly during the initial 14
7 days, and then tended to be stabilized at 22~45 L/m²·h without cleaning over two months of
8 operation. The results obtained implying that this innovative GDM process is prospective to offer
9 an opportunity to supply potable water through regenerating rainwater in decentralized
10 residences in an efficient, simple, and energy-free way.

11

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18

19 **Author Contributions**

20 C.S. (Lecturer) conceived the research goals, designed the methodology, conducted all the
21 experiments and wrote the manuscript. S.H. (Associate Professor) analyzed experimental data
22 and revised the manuscript. C.Q. (Associate Professor) revised the manuscript.

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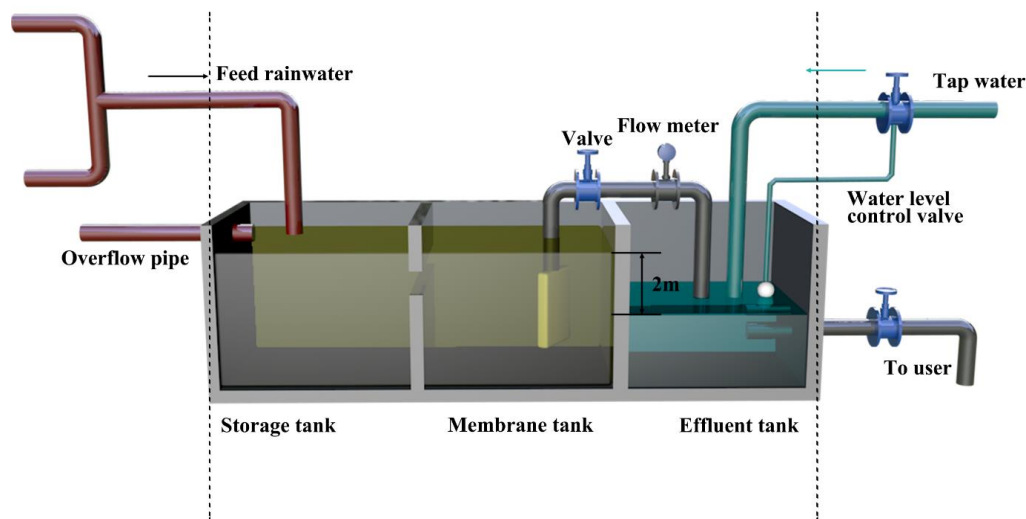
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14

15 **Fig. 1.** Experimental setup of the GDM unit.

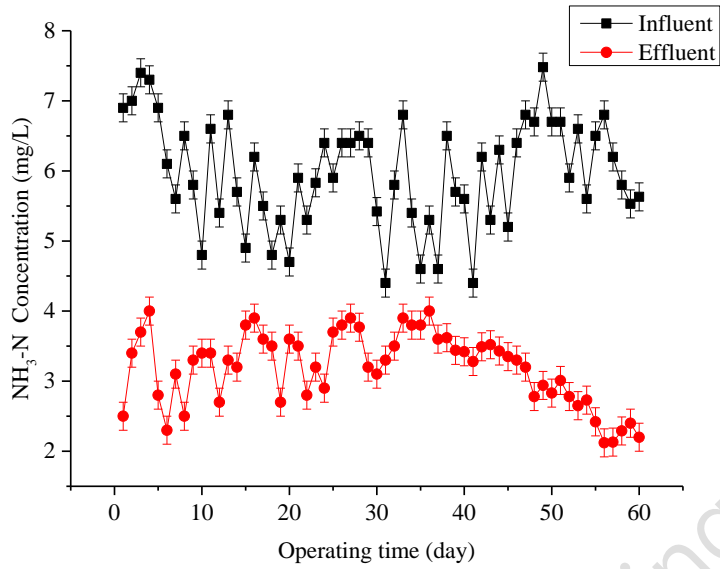
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2 **Table 1.** Rainwater and GDM Effluent Quality

Analytical Parameters	Feed Rainwater	GDM Effluent	CRWG limit	CDWG limit
Turbidity (NTU)	5.86 ± 1.64	0.46 ± 0.33	5	1
DOC (mg/L)	9.4 ± 3.86	2.17 ± 0.51	-	5
pH	7.4 ± 0.7	6.7-8.3	6.5~9	6.5~8.5
TDS (mg/L)	209 ± 172.4	17 ± 10.3	1,000	1,000
CODcr (mg/L)	35.9 ± 15.6	12.4 ± 4.4	50	5
NH ₃ -N	5.59 ± 2.89	3.21 ± 1.56	10	0.5
UV254 (cm ⁻¹)	0.087 ± 0.024	0.034 ± 0.018	-	0.060
E. coli (CFU/100mL)	330 ± 142	0~30	≤ 100	ND
Coliforms (CFU/100mL)	128 ± 37	0~9	≤ 100	ND

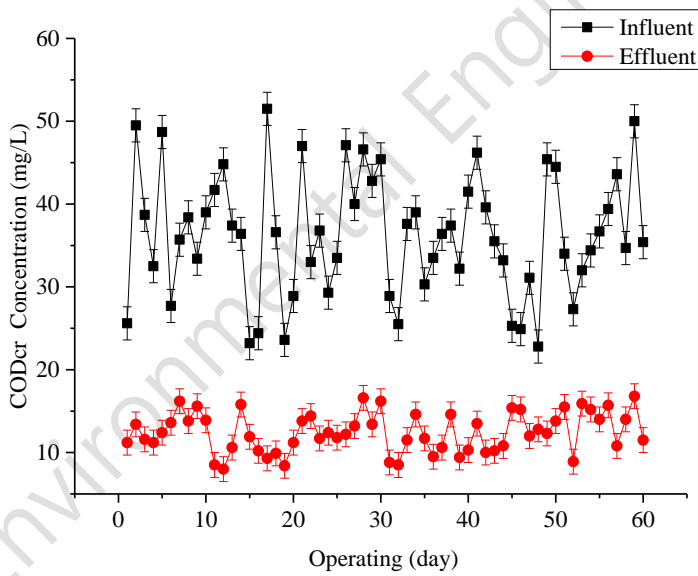
3 Note: ND represents “not detectable”

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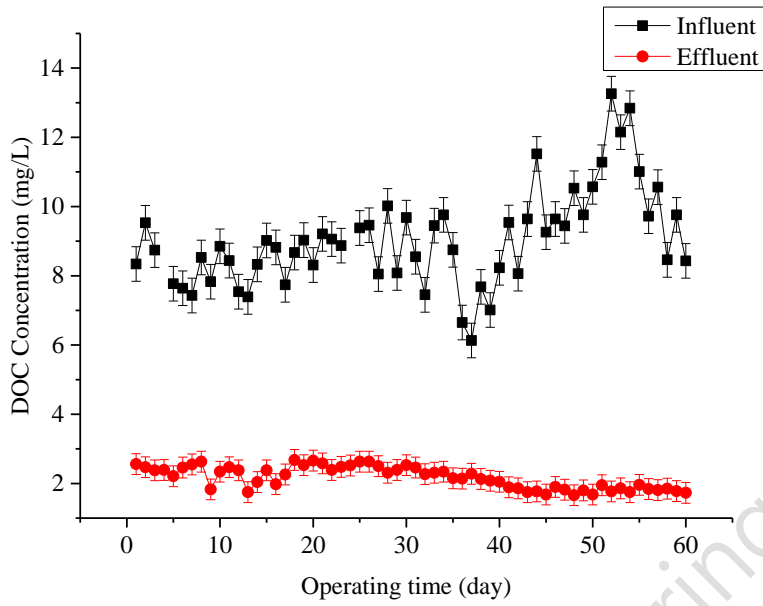
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2 **Fig. 2.** $\text{NH}_3\text{-N}$ removal of the GDM unit during operation period.



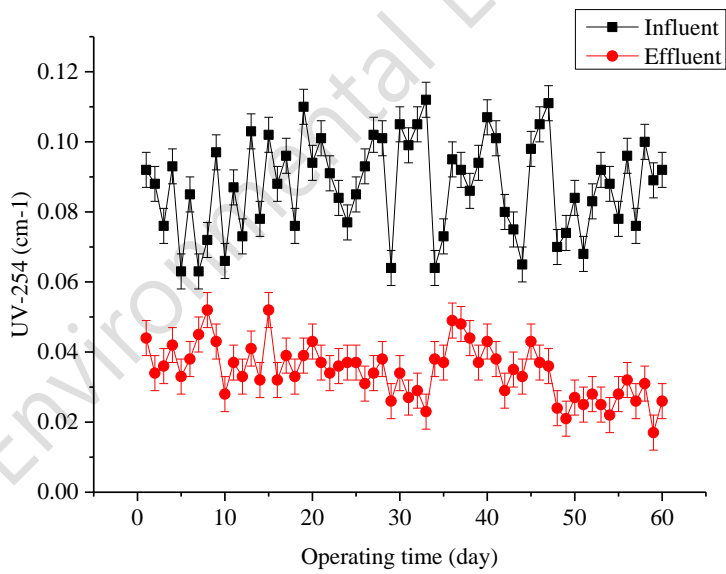
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4 **Fig. 3.** COD_{Cr} removal of the GDM unit during operation period.



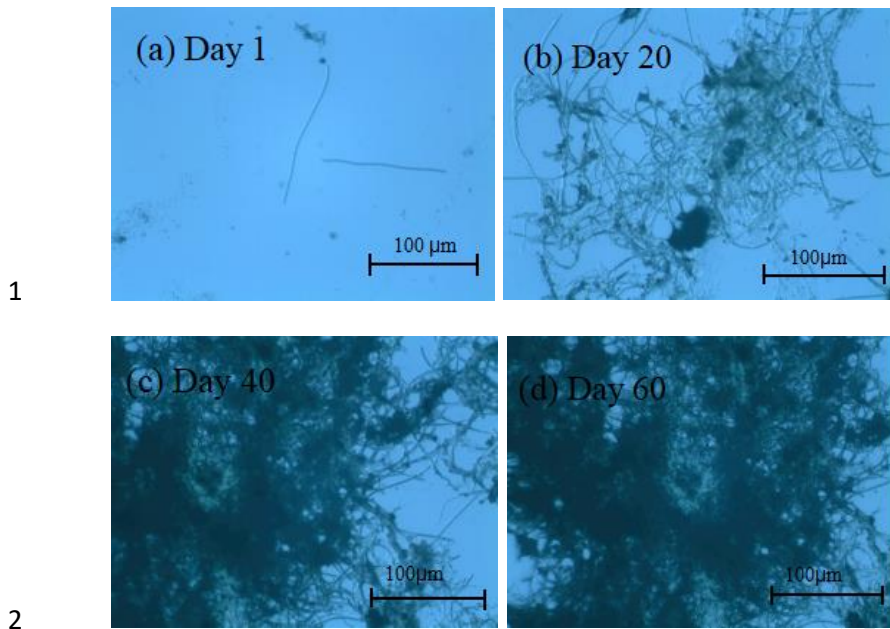
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Fig. 4. DOC removal of the GDM unit during operation period.

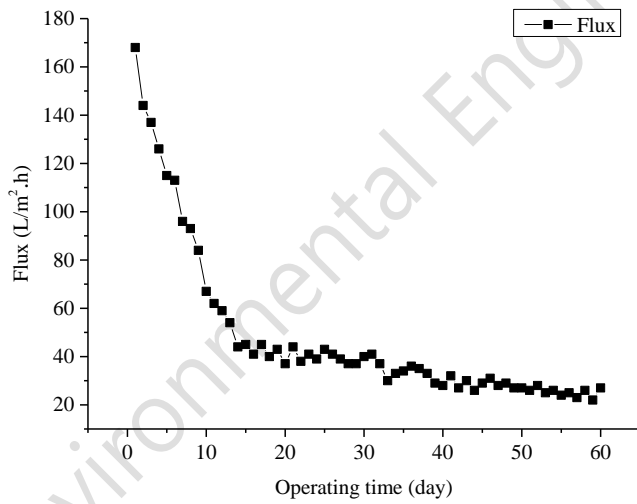


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Fig. 5. UV254 removal of the GDM unit during operation period.



3 **Fig. 6.** Microscopic images of microorganisms derived from the membrane surface.



5 **Fig. 7.** Membrane flux decline during 60 days experiment.

6

7